1	Soils consist of:										
А	grains and	В	water and air	С	void and	D	grains and water	E	particles and		
	particles		voids		spaces		voids only		air voids only		
2	The princip	les o	of soil mechanic	s are	2:						
A	a description of the basic soil properties.	В	denied the basic soil properties.	С	The application of soil properties to the solution of soil engineering problems	D	The use of the above soil structure properties to the solution of soil engineering problems.	E	solids and voids		
3	soil's mecha	nica	al properties are	e:							
A	strength.	В	stiffness.	C	permeability.	D	water content	E	clay percentages		
4	built on soil	pro	jects such as:			-	1				
A	foundation s, bridges, tunnels, roads	В	foundation, bridges, basement	С	foundation, bridges, buildings	D	tunnels, culverts, basements	E	Non of these		
5	the role of the void phase is:										
A	Chemical & physical Interaction	В	crushing the particles	C	bending the grains	D	all of these	E	Non of these		
6	The behavio	or of	the soil is one of	of th	e complicating c	hara	cteristics which de	epen	ds on:		
A	pressure	B	time	C	environment	D	all of these	E	non of these		
7	The role of	solic	l phase in soil n	ass	can explains as:						
A	loading reaction	В	increase solubility	С	increase the probability of quick sand	D	all of these	E	none of these		
8	The stabilit	y of	slopes depends	on		-	1				
А	height of the slope	В	weight of the soil	C	existence of water	D	uncounted forces	E	All of these		
9	The soil can	be	found:	T	ſ	r	I	1	r		
A	beside structures	В	above structures	C	below structures	D	structure itself	E	All of these		
10	The roles of	i voi	d in soil is								
A	Water erosion and pressure	В	influence the shear strength	C	Increase stability	D	Non of the above	E	A & B		
	Failure in a	n ex	travation is due	e to			N ₂ , C ₂ '1	Г	No. C.I		
A	Slope slip	В	i ype of water	C	water Scape	ם	No failure	E	Non of these		

12	The role of solid phase in soil mass can explains as:											
А	loading	В	increase the	С		D	non of the above	Е	A & B			
	reaction		probability of									
			quick sand									
13	GM symbol	me	ans:									
A	Gravelly	B	Clayey gravel	С	Gravelly silt	D	Silty gravel soil	Е	Non of these			
	clay soil		soil		soil		, <u>,</u> , , , , , , , , , , , , , , , , ,					
14	The maxim	um I	relationship bet	weel	n liquid limit and	d pla	sticity index is:		•			
А	A-Line	В	U-Line	С	Flow index	D	Effective	Е	Non of these			
							diameter					
1 =				41								
15	I ne parame	eter	which explains	the	real state of soll	IS:	DI	Б	Б			
A	PL	В	LL	C	LI		PI	E	E			
16	Amongst th	e cla	ay minerals, the	one	having the max	imun	n swelling tendenc	v is:				
Α	kaolinite	В	montmorillon	С	halloysite	D	illite	E	illite			
			ite						and montmor			
									illonite			
17	What is the name of soil type – according to its gradation – if the soil particles were											
Δ	relatively si		I In Size:	C	Wall graded	П	all of these	Б	Non of these			
A	graded soil	D	graded soil	C	wen graded	D	all of these	E	non or mese			
18	SP-SM mea	ns:	graded son	I				I				
A	poorly	В	poorly graded	С	uniformly	D	sandy silt	Е	Non of these			
	graded silt		silt		sand with silt							
	with sand											
1.0		Ļ										
19	If the soil sy	mb	ol is SP-SM, wh	ich o	of the following s	sente	nces is correct?:	F	N. C.I			
A	The sand	В	The silt	C	Ine	D	The fine soil	E	Non of these			
	the sample		soil is more		uniformly		under A-line					
	is well-		than clay		must be lower		under A-mie					
	graded		chair chay		than 6							
20	The rubber	-bal	loon test used w	ater	because water i	s		1				
А	Cheap	В	Have no	С	Incompressibl	D	All the above	E	Non of these			
			color and		e and							
			compressible		available							
21	AASHTO c	lassi	fication system	used	to classify soil	in:	A 11 /1 1	F	NT C.4			
A	highways	В	towers	C	slope stability	ען	All the above	E	Non of these			
22	According t	to Da	arcy's law for fl	ow f	hrough porous i	nedi	a. the velocity is pr	ODO	rtional to:			
A	effective	B	hydraulic	C	cohesion	D	angle of internal	E	Non of these			
	stress		gradient				friction					

23	the field pumping test to estimate the soil permeability are:										
А	confined	В	unconfined	С	auger hole test	D	inverse auger	E	A & B		
	flow test		flow test				hole test				
24	the hydraul	ic gi	radient in soils i	s rel	ated to:	-		-			
А	pressure,	В	pressure and	С	elevation head	D	pressure head	Е	Non of these		
	elevation		elevation		only		only				
	and		heads								
	velocity										
	heads										
25	The coeffici	ent	of permeability	can	be increased wit	h inc	crease in:				
А	particle	В	degree of	С	temperature	D	viscosity	E	A, B & C		
	size		saturation								
26	the water he	ead i	in the laborator	y pe	rmeability test n	nust	be for the	fine	soil particles.		
Α	dropped	В	fixed	С	changed incre	D	constant	Е	Non of these		
					asingly						
27	Which of th	e fo	llowing method	s is l	pest suited for de	eterm	ination of permea	bilit	y of coarse-		
	grained soil	s?				I	[I			
A	falling	В	constant head	С	falling or	D	Not constant	Е	Non of these		
	head test		test		constant tests		head test				
28	pumping-out seepage water from construction excavation is a function of;										
A	permeabilit	В	temperature	С	soil particle	D	deep	E	Non of these		
	У				size		groundwater				
20											
29	increasing in	n th	e degree of satu	ratio	on leading to:	D	· · · .		N. C.I		
A	increasing	в	decreasing in	С	increasing in	D	increasing in the	E	Non of these		
	in the soil		the		the volume of		water content				
	permeabilit		coefficient of		the soil						
	У		SOII		particle						
20	a a fisiant a	fac	permeability	(1-) :	a denendent en						
<u> </u>	coefficient o		n permeability		degree of	П	fluid	Б	All of these		
A	son grans	Б	distribution	C	degree of	D	abaractoristics	E	All of these		
31	size	flor			saturation		characteristics				
	no change	R	no change in	C	flow velocity	П	All of these	Б	Non of these		
A	in flow	Б	flow velocity	C	changes with	D	All of these	Ľ	Non of these		
	velocity		with distance		time and/or						
	with time		with distance		distance						
32	the velocity	hea	d from fluid flo	w in	the soil is elimin	ated	due to:				
	small	R	the flow is		high velocity		been forgotten	F	Non of these		
1	velocity	ם	slow		mgn velocity						
33	best compa	rted	soil hannened v	vher	the soil is	1		L			
A	drv	R	fully	C	having coarse	D	having	E	Non of these		
**			saturated		grains	2	minimum void				
			Saturated		Siding		ratio				
34	Choose the	mos	t suitable comp	acte	r to compact a tr	ench	with width equal	to 1	.5m filled		
	with soil cla	ssifi	ed as CM.			chief	and the second s				

А	Rammer	В	Sheep-Foot	С	Nuclear	D	Hand-Held	Е	Non of these
			Roller		machine		Vibrating Plate		
35	Rise of wate	er ta	ble above the g	roun	d surface causes	•••	I		
Α	increase in	В	increase in	С	decrease in	D	All of these	Ε	Non of these
	total stress		effective		effective stress				
36	with water (table	stress	offoo	tivo stross will			1	
30 A	decreases		increases		decreases then		All of these	F	Non of these
Λ	uccicases	D	mercases	C	increases	D	All of these		Non of these
37	No. of flow	char	nels is	-	mercuses	l		I	
A	Nd	В	Nf	С	Н	D	ht	E	Ic
38	No. of head	dro	ps is		T		-		
A	ht	В	ie	С	Nf	D	Nd	Е	Н
20			· · · · · · · · · · · · · · · · · · ·		<u>بالمحمد معمد المحمد المحمد</u>			1	
39	critical hyd		ic gradient (from	m so	ht properties)	D	TT	F	Nd
A	IC	D	le	C	m	D	п	E	ING
40	water head	(ht-]	he) is					1	
A	he	В	Н	C	ht	D	hp	Е	U
							1		
41	exit hydrau	lic g	radient (from w	vater	flow) is			-	
A	ic	В	ht	C	Н	D	ie	E	Nf
12	The shape of	fol	v porticlo is us	مال	7•			1	
42 Δ	elongated	R R	upflaky		sheets	D	All of these	E	Non of these
Λ	cioligateu							I H	
		2	uiiiiaky		Sheets	D	All of these	E	Non of these
1		D	unnaky	C	Sheets	D	All of these	E	i ton or these
43	The particle	es ar	e deposited to f	orm	sedimentary soi	D I due	e to	E	Troll of these
43 A	The particle velocity	es ar B	e deposited to f	orm C	sedimentary soi electrolyte	D I due D	All of these All of these	E E	Non of these
43 A	The particle velocity reduction	es ar B	e deposited to f solubility decrease	orm C	sedimentary soi electrolyte increase	D I due D	All of these All of these	E	Non of these
43 A 44	The particle velocity reduction The types o	es ar B f soi	re deposited to f solubility decrease	orm C ne m	sedimentary soi electrolyte increase ethod of weathe	D I due D ring	All of these	E	Non of these
43 A 44 A	The particle velocity reduction The types of coarse	es ar B f soi	e deposited to f solubility decrease l according to th fine grained	orm C he m	sedimentary soi electrolyte increase ethod of weathe coarse grained	D I due D ring D	All of these All of these All of these	E E E	Non of these
43 A 44 A	The particle velocity reduction The types of coarse grained	es ar B f soi	e deposited to f solubility decrease I according to t fine grained	orm C he m	sedimentary soi electrolyte increase ethod of weathe coarse grained and fine	D l due D ring D	All of these All of these All of these	E E E	Non of these Non of these
43 A 44 A	The particle velocity reduction The types of coarse grained	es ar B f soi B	re deposited to f solubility decrease I according to the fine grained	orm C he m	sedimentary soi electrolyte increase ethod of weathe coarse grained and fine grained	D l due D ring D	All of these All of these All of these	E E E	Non of these
43 A 44 A	The particle velocity reduction The types of coarse grained	es ar B f soi B	e deposited to f solubility decrease l according to th fine grained	orm C he m C	sedimentary soi electrolyte increase ethod of weathe coarse grained and fine grained	D I due D ring D	All of these All of these All of these	E E E	Non of these
43 A 44 A 45	The particle velocity reduction The types of coarse grained When the p	es ar B f soi B rodu	re deposited to f solubility decrease l according to th fine grained	orm C he m C	sedimentary soi electrolyte increase ethod of weathe coarse grained and fine grained ing are not trans	I due D ring D sport	All of these All of these ted as sediments b	E E E	Non of these Non of these emain in
43 A 44 A 45 A	The particle velocity reduction The types of coarse grained When the p place, the so alluvial	es ar B f soi B rodu pil is B	e deposited to f solubility decrease l according to th fine grained icts of rock wea : residual	orm C he m C ther	sedimentary soi electrolyte increase ethod of weathe coarse grained and fine grained ing are not trans	D I due D ring D sport	All of these All of these ted as sediments b fill	E E E Dut ro	Non of these Non of these emain in Non of these
43 A 44 A 45 A	The particle velocity reduction The types of coarse grained When the p place, the so alluvial	es ar B f soi B rodu pil is B	re deposited to f solubility decrease l according to th fine grained	orm C he m C ither	sedimentary soi electrolyte increase ethod of weathe coarse grained and fine grained ring are not trans	I due D ring D sport	All of these All of these ted as sediments b fill	E E E E E	Non of these Non of these emain in Non of these
43 A 44 A 45 A 45	The particle velocity reduction The types of coarse grained When the p place, the so alluvial	es ar B f soi B rodu jil is B	re deposited to f solubility decrease l according to th fine grained icts of rock weat: residual	orm C he m C ither	sedimentary soi electrolyte increase eethod of weathe coarse grained and fine grained ring are not trans glacial	I due D ring D sport	All of these All of these All of these ted as sediments h	E E E E E	Non of these Non of these Remain in Non of these
43 A 44 A 45 A 45 A	The particle velocity reduction The types of coarse grained When the p place, the so alluvial The weather size of soil	es ar B f soi B rodu oil is B ring B	re deposited to f solubility decrease l according to the fine grained icts of rock weat residual of parent rocks	form C he m C ither	sedimentary soi electrolyte increase ethod of weathe coarse grained and fine grained fing are not trans glacial ects on	I due D ring D sport D	All of these All of these All of these fill All of these	E E E E E E	Non of these
43 A 44 A 45 A 46 A	The particle velocity reduction The types of coarse grained When the p place, the so alluvial The weather size of soil particles	es ar B f soi B rodu jil is B ring B	re deposited to f solubility decrease l according to th fine grained icts of rock weat: residual of parent rocks sedimentatio n velocity	ither	sedimentary soi electrolyte increase eethod of weathe coarse grained and fine grained ring are not trans glacial ects on transportation of soil	I due D ring D sport	All of these All of these All of these ted as sediments h fill All of these	E E E E E E	Non of these Non of these emain in Non of these Non of these

А	soil	В	vertical	С	strength from	D	All of these	Е	Non of these			
	strength		permeability		cementing and							
	from faults				bonding							
48	Sediments of	an l	pe transported l	oy:		_						
A	water	В	air	С	ice	D	gravity	Е	All of these			
49	When the products of rock weathering are not transported as sediments but remain in											
	place, the so	oil is	:									
Α	residual	В	glacial soil	С	Sedimentary	D	All of these	E	Non of these			
	soil				Soil							
		<u> </u>										
50	In the floce	ulate	ed structure in s	soils,	the particles are	e:						
A	parallel	В	edge to face	C	face to face	D	All of these	E	Non of these			
51	Dispersed t	ype	of soil structure	is a	n arrangement c	omp	rising particles ha	ving				
A	edge to	В	edge to edge	С	face to face or	D	All of these	E	Non of these			
	face		orientation		parallel							
	orientation				orientation	<u>ا</u>						
52	It is one of	the l	aboratory meth	ods	to find the shear	stre	ngth parameters (
A	triaxial test	B	SPT	C	Oedometer	D	permeameter	E	Non of these			
53	The symbol of the excess pore water pressure immediately after the application of the load											
	is:	D				5	1.					
A	ue	В	uo		uss	D	h	E	Н			
54	Physical pro	oper	ties of a permea	ant v	which influence p	berm	eability are:		N. C.I			
A	viscosity	В	both viscosity	C	unit weight	D	All of these	E	Non of these			
	only		and unit		only							
55	Quick sand	ic o	weight									
<u>33</u> Δ	type of	IS A	flow	С	flow condition	р	flow condition	F	Non of these			
Л	sand	Ъ	condition	C	occurring in		occurring in		Non of these			
	Sand		occurring in		cohesionless		both cohesive					
			cohesive soils		soils		and cohesionless					
			•••••••••••		50110		soils					
56	Sand partic	les a	re made of	••		1						
Α	rock	В	kaolinite	С	illite	D	montmorillonite	E	Non of these			
	minerals											
57	According (to Da	arcy's law for fl	ow t	hrough porous r	nedia	a, the velocity is p	opo	rtional to:			
А	cohesion	В	angle of	С	hydraulic	D	effective stress	E	Non of these			
			internal		gradient							
			friction									
58	The quantit	ty of	seepage under	••••	and sheet pi	ling	can be estimated u	sing	the graphical			
	construction	n kn	own as a flown	et.	1							
A	Hydropow	В	Hydroelectric	C	Water turbine	D	Dam	E	Non of these			
	er		ity									
59	k has the u	nits 1	m/s and is the a	vera	ge velocity of wa	ter p	bassing through a p	poro	us medium			
	under a uni	t						T				
A	Pelton	В	Hydraulic	C	Hydroelectrici	D	Dam	E	Non of these			
<i>(</i>)	wheel		head	<u> </u>	ty							
60	Which of th	e fo	llowing method	s is l	pest suited for la	bora	tory determination	n of j	permeability			

	of fine-grained soils?										
А	falling or	В	falling head	С	constant head	D	pumping	Е	auger hole		
	constant		test		test						
	tests										
61	What happ	ens t	to the volume of	the	solid grains whe	en so	il is compacted?				
Α	Decreases	В	nothing	С	increases	D	extended	Е	Non of these		
62	From soil st	truct	<u>tural features is</u>	••••	••						
А	Lenses	В	Fissures	С	Bonding	D	All of these	Е	Non of these		
63	for flownet in Figure 1, the number of flow channels is:										
A	4	В	6	C	8	D	9	E	10		
<u> </u>	0 01 /			<u> </u>							
64	for flownet	In F	igure 1, the num	nber	of drops is:	D	10		1.1.1		
A		В	5	C	9	D	10	E	11		
65	for flormat	in F	jauna 1 tha haa	4 4:4	fformer og (II) igt						
05	2.5		Igure 1, the nea		Terence (H) IS:	П	10	Б	11		
A	5.5	D	5.5	C	1.5		10	E	11		
66	for flownot in Figure 2, the number of flow channels is:										
Δ	5	R	$\frac{1}{3}$	C		D	10	F	11		
11	5	D	5	C	1		10		11		
67	for flownet in Figure 2, the number of drops is:										
Α	5	В	7	С	9	D	10	Е	11		
68	for flownet in Figure 2, the head difference (H) is:										
А	50	В	40	C	70	D	100	E	110		
(0)	0 01 (Ļ		۱ <u>.</u>					
69	for flownet	in F	igure 3, the num	nber	of flow channel	S IS:	10	-			
A	8	В	6	С	4	D	10	E	11		
70	e. e	•	•	. 1							
70	for flownet		igure 3, the num	nber	of drops is:	D	10	Б	11		
A	4	В	0	C	8	D	10	E	11		
71	for flownet	in F	joure 3 the hea	d di	fference (H) is:						
	3	R	$\int A$		5 25	П	10	F	11		
Λ	5	D	+	C	5.25		10	Ľ	11		
72	for flownet	in F	igure 4. the num	nber	of flow channel	s is:		L			
Α	2	В	7	C	6	D	4	Е	10		
73	for flownet	in F	igure 4, the num	nber	of drops is:		•				
А	2	В	4	С	6	D	8	Е	10		
74	for flownet	in F	igure 4, the hea	d di	fference (H) is:						
A	5	B	7	C	9	D	10.5	E	12		
		Ļ			 						
75	a clay layer	who	ose total settlem	ent I	under a given loa	ad is	expected to be 25	mm	, settles by		
	50mm in 15	day	s, the average c	legro	ee of consolidatio)n (U	$(\mathbf{a}) =$				

A	40%	В	20%	C	70%	D	80%	E	90%			
76	a clay layer whose total settlement under a given load is expected to be 250mm, settles by											
	150mm in 1	25 d	lays, the averag	e de	gree of consolida	tion	(Ua) =					
А	40%	В	60%	С	70%	D	80%	E	90%			
77	for degree o	of co	nsolidation of 5	0%,	the time factor ((Tv)	=		•			
А	0.2	В	0.197	C	0.1	D	0.15	E	0.25			
78	for degree of consolidation of 90%, the time factor (Tv) =											
А	0.680	В	0.848	C	0.800	D	0.480	E	0.860			
79	the total settlement of a clay is expected to be 200mm, settles by 20mm in two weeks, the											
	average degree of consolidation (Ua) =											
А	50%	В	40%	С	10%	D	30%	E	20%			
80	the total set	tlem	ent of a clav is	expe	cted to be 200m	m. se	ettles by 50mm in s	six m	onths, the			
	average degree of consolidation (Ua) =											
А	35%	В	45%	Ċ	25%	D	50%	E	60%			
81	e e	1 – e	2			I		I				
	$Cc = \frac{1}{\log \sigma}$	′ ₂ −1	ogo'			I	1	I				
Α	Coefficient	В	Expansion	С	Compression	D	Coefficient of	Е	Non of these			
	of Volume		Index		Index		Compressibility					
	Change											
82	$(e_0 - e1)$											
	$u_v = (\sigma'_1)$	$-\sigma$	')									
A	Coefficient	В	Expansion	C	Compression	D	Coefficient of	Е	Non of these			
	of Volume	_	Index		Index	-	Compressibility	_				
	Change											
83	1											
	$m_{v} = \frac{1}{1}$		ı _v									
	1+	eo				1 _		1				
A	Coefficient	В	Expansion	C	Compression	D	Coefficient of	Е	Non of these			
	of Volume		Index		Index		Compressibility					
Q /	Change											
04	Cr = Ce =		Δe									
	_	Δl	ogơ'									
А	Coefficient	В	Expansion	C	Compression	D	Coefficient of	Е	Non of these			
	of Volume		Index		Index		Compressibility					
	Change											
85	Cv. t											
	$Tv = \frac{1}{d^2}$											
A	Emeraria -	р	time for t	C	Company	D	Coefficient	P	Nor - f (1			
A	Expansion	В	time factor	C	Compression	ם	Commence it it it	E	inon of these			
	index				maex		Compressibility					

86	$Ua = \frac{Sc_{tin}}{Sc_{to}}$	<u>me</u> tal	100							
A	Expansion Index	В	average degree of consolidat	ion C	Compression Index	D	Coefficient of Compressibility	E	Non of these	
87	$\sigma = \gamma$.	Ζ								
A	Total stress in homogene ous soil	В	Total stres below a riv or lake	s C ver	Total stress in multi-layered soil	D	pore pressure	E	Non of these	
88	$k = \frac{\sigma_h}{\sigma_v}$	$k = \frac{\sigma_h}{\sigma_v}$								
A	Coefficient of Lateral Stress	В	Total stres below a riv or lake	s C ver	Coefficient of permeability	D	pore pressure	E	Non of these	
89	$\sigma_{\rm v} = \gamma .z + \gamma_{\rm w} .z_{\rm w}$									
A	Total stress below a river or lake	В	Total stres in multi- layered so	s C il	Coefficient of permeability	D	pore pressure	E	Non of these	
90	$\mathbf{u} = \gamma_{w}$.h _v	v							
A	pore pressure	В	Total stres in multi- layered so	s C il	Coefficient of permeability	D	Total stress below a river or lake	E	Non of these	
91	$\sigma' = \sigma t$	— 1	и							
A	Effective stress	В	Total stres in multi- layered so	s C il	Coefficient of permeability	D	Total stress below a river or lake	E	Non of these	
92	$\frac{\sigma_{total}}{u} > 1$									
A	Effective stress	В	Factor of safety again boiling condotion	ins C	Coefficient of permeability	D	Total stress below a river or lake	E	Non of these	
93	$\Delta \sigma_{\rm v} = \frac{\Delta}{(B+T)^2}$	Δq* - Z)	$\frac{B * L}{* (L + Z)}$							
A	Total stress below a river or lake	В	Increase in total stress from rectangula footing	r C	Total stress in multi-layered soil	D	pore pressure	E	Non of these	

94	major principal stress is											
А	σt	В	σ1	С	σh	D	σ3	E	Non of these			
95	minor principal stress is											
А	σt	В	σ 3	C	σh	D	σ1	E	Non of these			
96	$\frac{\sigma_1-\sigma_3}{2}$											
A	σh	В	Center of the circle	С	Radius of Mohr circle	D	σ3	E	σ1			
97	$\left[\frac{\sigma_1 + \sigma_3}{2}\right]$											
Α	σh	В	σt	С	Center of the circle	D	Radius of Mohr circle	E	σ1			
98	the angle of	inte	ernal friction is									
Α	α	В	σ	С	Φ	D	γ	E	Δ			
99	$\tau = C +$	σt	an D									
A	Center of the circle	В	Radius of Mohr circle	С	Failure Envelope	D	σ1	E	σt			
100	$\sigma_1 - \sigma_3$							-				
А	normal stress	В	shear strain	С	deviator stress	D	σ1	E	σt			







